

SOME PLANE ADIABATIC IDEAL GAS FLOWS
CONTAINING SHOCKS

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We obtain the solution describing adiabatic flows of an ideal gas characterized by the two parameters a and b such that

$$[a] = L^{m+1}T^{-1}, \quad [b] = ML^{-2-2m}$$

where m is arbitrary ($m > 0$). This solution permits the construction of flows containing shocks.

1. Assume that in the region $y > 0$ an ideal (i.e., without viscosity and thermal conductivity) perfect gas travels parallel to the Ox -axis and has the following parameters:

$$p \equiv 0, \quad v \equiv 0, \quad u = u_0(y) = ay^{-m}, \quad \rho = \rho_0(y) = by^{2m-1} \quad (1.1)$$

and passes through a normal shock. The conditions on the shock have the form [1]

$$u = \frac{\gamma-1}{\gamma+1}u_0, \quad v = 0, \quad \rho = \frac{\gamma+1}{\gamma-1}\rho_0, \quad p = \frac{2}{\gamma+1}\rho_0u_0^2 \quad (1.2)$$

In view of the presence of the pressure gradient in the direction of the Oy -axis, the flow behind the normal shock is described by the system of equations [2]

$$\frac{\partial}{\partial \eta} \frac{v}{u} + v \frac{\partial}{\partial \xi} \frac{v}{u} + p \frac{\partial}{\partial \xi} \frac{1}{\rho u} = 0, \quad \frac{\partial}{\partial \eta} \frac{1}{p} + \frac{\partial}{\partial \xi} \frac{v}{p} = 0 \quad (1.3)$$

$$\frac{u^2 + v^2}{2} + \frac{\gamma}{\gamma-1} \frac{p}{\rho} = i_0(\eta), \quad p = \rho^\gamma f_0(\eta)$$

Here u and v are the velocity components along the Ox - and Oy - axes, respectively; p is pressure; ρ is density; $\gamma > 1$ is the adiabatic exponent; f_0 and i_0 are arbitrary functions. The independent variables ξ (the function introduced by Martin [3]) and η (the stream function) are defined by

$$d\xi = \rho u v dy - (p + \rho v^2) dx, \quad d\eta = \rho u dy - \rho v dx \quad (1.4)$$

The constants a and b in (1.1) and the variables ξ and η have the following dimensions:

$$[a] = L^{m+1}T^{-1}, \quad [b] = ML^{-2-2m}, \quad [\xi] = MT^{-2}, \quad [\eta] = ML^{-1}T^{-1} \quad (1.5)$$

Therefore the only dimensionless parameter is the quantity $s = \xi a^{-2} b^{-1}$, and the functions in (1.3) can be written in the form

$$u = a^2 b \eta^{-1} U(s), \quad v = a^2 b \eta^{-1} V(s), \quad s = \xi a^{-2} b^{-1} \quad (1.6)$$

$$p = \eta^{-1/m} a^{(2m+1)/m} b^{(m+1)/m} P(s), \quad \rho = \eta^{(2m-1)/m} a^{(1-2m)/m} b^{(1-m)/m} R(s)$$

The dimensionless functions U , V , P , and R satisfy the system of equations obtained from (1.3),

$$\frac{1}{P} + m \left(\frac{V}{P} \right)'_s = 0, \quad V \left(\frac{V}{U} \right)'_s + P \left(\frac{1}{RU} \right)'_s = 0$$

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$$\frac{U^2 + V^2}{2} + \frac{\gamma}{\gamma - 1} \frac{P}{R} = H^2, \quad P = (RC_1)^\gamma \quad (1.7)$$

Here H and C_1 are arbitrary constants (the functions f_0 and i_0 are defined to within a constant factor). The stream function η does not undergo a discontinuity upon passing through the shock. Therefore

$$d\eta = \rho_0 u_0 dy = aby^{m-1} dy$$

Hence

$$y^m = m\eta(ab)^{-1}$$

Since the image of the shock in the $\xi\eta$ -plane is the line $s = 0$ [2], we write conditions (1.2) for the functions U , V , P , and R in the form

$$\begin{aligned} U|_{s=0} &= \frac{\gamma-1}{(\gamma+1)m}, \quad V|_{s=0} = 0 \\ R|_{s=0} &= \frac{\gamma+1}{\gamma-1} m^{(2m-1)/m}, \quad P|_{s=0} = \frac{2}{\gamma+1} m^{-1/m} \end{aligned} \quad (1.8)$$

Solving (1.7) and using (1.8), we find

$$\begin{aligned} U &= \frac{1}{m} - \frac{\gamma+1}{\gamma-1} m\tau, \quad V = \left(\frac{2}{\gamma-1} \tau - \left(\frac{\gamma+1}{\gamma-1} \right)^2 m^2 \tau^2 \right)^{1/2} \\ P &= \tau R, \quad R = \frac{\gamma+1}{\gamma-1} m^{(2m-1)/m} \left(\frac{\tau}{\tau_1} \right)^{\gamma/(\gamma-1)}, \quad \tau_1 = \frac{2(\gamma-1)}{(\gamma+1)^2 m^2} \end{aligned} \quad (1.9)$$

$$s = m \frac{\gamma+1}{(\gamma-1)^2} \int_{\tau_1}^{\tau} \frac{1}{V(\tau)} \left(1 - \frac{\gamma+1}{\gamma-1} m^2 \tau \right) d\tau$$

The equations of the streamlines behind the shock can be written in parametric form (taking the shock as the Oy -axis)

$$\begin{aligned} x &= - \left(\frac{m}{ab} \right)^{1/m} h \eta^{1/m} \int_{\tau_1}^{\tau} \frac{\gamma-1 - (\gamma+1)m^2 z}{V(\gamma-1)2z - (\gamma+1)^2 m^2 z^2} z^{-\gamma/(\gamma-1)} dz, \quad h = \frac{\tau_1^{\gamma/(\gamma-1)}}{(\gamma-1)m} \\ y &= - \left(\frac{m}{ab} \right)^{1/m} h m \eta^{1/m} \int_{\tau_1}^{\tau} \frac{\gamma-1 - (\gamma+1)m^2 z}{V(\gamma-1)^2 - 2(\gamma^2-1)m^2 z + (\gamma+1)^2 m^2 z^2} z^{-\gamma/(\gamma-1)} dz + \left(\frac{m}{ab} \right)^{1/m} \eta^{1/m} \end{aligned} \quad (1.10)$$

Thus, (1.6), (1.9), and (1.10) completely describe the gas flow behind a normal shock.

Directly behind the shock $V(\tau_1) = 0$. Therefore, with motion along any streamline $\eta = \text{const}$ downstream from the shock τ decreases from τ_1 (at the shock) to 0, and $V \rightarrow 0$, $x, y \rightarrow \infty$ as $\tau \rightarrow 0$. We denote by α the slope of the streamlines to the Ox -axis. Behind the shock $\alpha = 0$, as we move downstream α increases to some value α_{max} and then decreases to 0. It is not difficult to show using (1.9) that the value α_{max} , corresponding to the inflection point on the streamline, is independent of η and is reached for $\tau = \tau_*$, where

$$\tau_* = \frac{\gamma-1}{\gamma(\gamma+1)m^2}, \quad \lg \alpha_{\text{max}} = \frac{1}{V\gamma^2-1}$$

We further find from (1.9)

$$M^2 = \frac{u^2 + v^2}{\gamma p} \rho = \frac{\gamma-1-2\gamma m^2 \tau}{\gamma(\gamma-1)m^2 \tau}, \quad M(\tau_*) = 1$$

Hence, and also from (1.10), we see that the lines along which $M = \text{const}$ are straight lines passing through the coordinate origin. Specifically, the sonic line ($M = 1$) of the flow behind the shock is a straight line

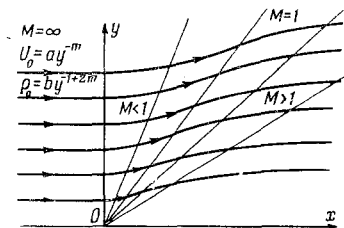


Fig. 1

and the locus of points of inflection of the streamlines behind the shock (Fig. 1). Taking any line $\eta = \text{const}$ as the wall, we obtain the flow past a curvilinear contour.

2. Let us assume that a gas having parameters (1.1) passes through an oblique rectilinear shock.

Using the known relations for a strong oblique shock [1], we can show that the flow behind the shock is described as before by solution (1.9), in which τ_1 is to be replaced by $\tau_1 \sin^2 \beta$, where β is the slope of the shock to the Ox-axis. This means that in the flow shown in the figure any straight line $y = kx$ can be taken as the oblique shock.

On the basis of the solution obtained here and using the substitution principle [4], we can construct non-self-similar adiabatic flows containing shocks.

LITERATURE CITED

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